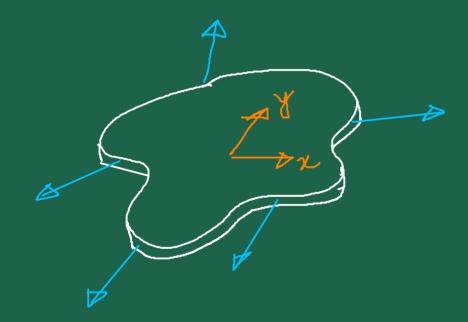
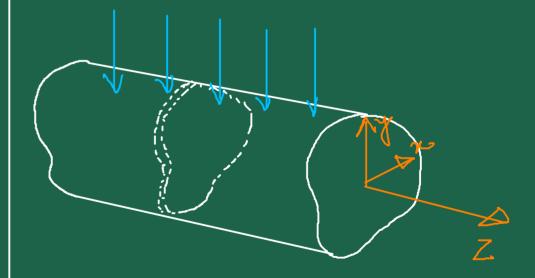
## Plane Stress



$$\sigma_{zz} = \sigma_{zx} = \sigma_{yz} = 0$$

$$\sigma_{ny} = \sigma_{ny}(x,y), \sigma_{nx} = \sigma_{nn}(x,y), \sigma_{ny} = \sigma_{ny}(x,y)$$

## Plane Strain



$$u = u(x, y) \qquad W = 0$$

$$V = v(x, y)$$

## Plane Stross

Lane Strob

$$\begin{aligned}
&\mathcal{E}_{nn} = \frac{1}{P} \left( G_{nn} - \mathcal{S}(G_{yy} + \mathcal{J}_{zz}) \right) \\
&\mathcal{E}_{yy} = \frac{1}{P} \left( G_{yy} - \mathcal{S}(G_{nn} + \mathcal{J}_{zz}) \right) \\
&\mathcal{E}_{zz} = \frac{1}{P} \left( \mathcal{J}_{zz} - \mathcal{S}(G_{nn} + G_{zz}) \right) \\
&\mathcal{E}_{nn} = \frac{1}{2G} \left( \mathcal{J}_{zz} - \mathcal{S}(G_{nn} + G_{zz}) \right) \\
&\mathcal{E}_{nn} = \frac{1}{2G} \left( \mathcal{J}_{zz} - \mathcal{S}(G_{nn} + G_{zz}) \right) \\
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&\mathcal{E}_{zz} = \frac{1}{2G} \left( \mathcal{J}_{zz} - \mathcal{J}_{zz} - \mathcal{J}_{zz} \right) \\
&\mathcal{E}_{zz} = \frac{1}{2G} \left( \mathcal{J}_{zz} - \mathcal{J}_{zz} - \mathcal{J}_{zz} \right) \\
&\mathcal{E}_{zz} = \frac{1}{2G} \left( \mathcal{J}_{zz} - \mathcal{J}_{zz} -$$

$$\begin{aligned} \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \left[ \int_{NA} - \lambda \int_{NA} \right] \\ \xi_{NA} &= \frac{1}{E} \left[ \int_{NA} - \lambda \int_{NA} \left[ \int$$

Plane Strain  $\xi_{1} = \frac{1}{E} \left[ \zeta_{1} - \lambda \left( \zeta_{1} + \zeta_{2} \right) \right] \rightarrow \xi_{1} = \frac{1}{E} \left( \zeta_{1} - \lambda \zeta_{1} - \lambda \zeta_{1} - \lambda \zeta_{1} \right) \\
= \frac{1+\lambda}{E} \left[ \left( 1 - \lambda \right) \zeta_{1} - \lambda \zeta_{1} \right]$ Eyy = [ [ [ ] - [ ( ] ( ] + ( ] ) ]  $\Rightarrow \xi_{yy} = \frac{1+2}{F} \left[ 1-3 \right) \mathcal{I}_{yy} - 5 \mathcal{I}_{nn}$  $0^{1/2} = \frac{1}{E} \left[ \sigma_{zz} - \lambda (\sigma_{xx} + \sigma_{yy}) \right]$ Jan 76, Jy 70 Jzz 20 > 0 = 5 ( In + Cyx)  $\frac{\mathcal{E}_{xy}}{0 \mathcal{R}_{yz}} = \frac{1}{24} \mathcal{I}_{yz}$   $0 \mathcal{R}_{yz} = \frac{1}{24} \mathcal{I}_{yz} \Rightarrow \mathcal{I}_{yz}^{zz} \Rightarrow$ Ty FD Jz = Jz = 0  $\sigma \mathcal{L}_{22} = \frac{1}{25} \mathcal{L}_{2x} = \mathcal{L}_{2x} Z \mathcal{L}$ 

## **Airy Stress Function**

For Plane Stoop problems
$$\mathcal{T}_{xz} = \mathcal{T}_{yz} = \mathcal{T}_{zz} = 0$$

Strons egps egms

$$\frac{\partial V_{x}}{\partial x} + \frac{\partial V_{y}}{\partial y} = \frac{\partial V_{x}}{\partial x}$$

$$\frac{\partial V_{x}}{\partial x} + \frac{\partial V_{y}}{\partial y} = \frac{\partial V_{x}}{\partial x}$$

$$\frac{\partial V_{x}}{\partial x} + \frac{\partial V_{y}}{\partial y} = \frac{\partial V_{x}}{\partial x}$$

Arbitrary choices of the Arry Stress for are MOT allowed!

Information from the compatibility caps must be embedded within

the mathematical formulation of the Stress for approach.

Compatibility equal Constitutive Rebr.

$$\frac{3\xi_{nn}}{3\eta^n} + \frac{3\xi_{ny}}{3\eta^n} = 2\frac{3\xi_{ny}}{3\eta^n} \leftarrow \text{Stross eqb. equal }$$
 $\left(\frac{3}{3\eta^n} + \frac{3}{3\eta^n}\right)\left(\frac{3}{3\eta^n} + \frac{3}{3\eta^n}\right)\left(\frac{3}{3\eta^n} + \frac{3}{3\eta^n}\right) = 0$ 

$$\Rightarrow \left(\frac{5}{200} + \frac{5}{200}\right) \left(\frac{50}{200} + \frac{5}{200}\right) = 0$$

$$= \sqrt{\frac{\delta}{\delta x} + \frac{\delta}{\delta y}} \left( \frac{\delta}{\delta x} + \frac{\delta}{\delta y} \right) \left( \frac{\delta}{\delta x} + \frac{\delta}{\delta y} \right) q = 0$$

$$\frac{\sqrt{4} \varphi = 0}{\sqrt{3} \varphi + 2 \frac{\sqrt{3} \varphi}{\sqrt{3} \sqrt{3}} + \frac{\sqrt{3} \varphi}{\sqrt{3} \sqrt{4}} = 0$$

VI: Biharmonic operator

Operational Steps: # Assume some general sol forms for of

# Conditions that must be satisfied for the general soln form to satisfy \(\forall fz\)

# Satisfy the boundary conditions

Usual to consider polynomial forms for of  $\# \varphi = const. \rightarrow \forall \varphi = 0 \lor$ Jun = Juny = Jyy = 0 g=Ar, Ay, An+By -> Tropzou Jun z Jung = Jung = 0 Q = Ay -> FIQZOW 

$$\sigma_{m} = \frac{\partial \varphi}{\partial y} Z A = \frac{T}{\alpha}$$

$$cf Z A y^{2} = \frac{T}{\alpha} y^{2} Y$$

$$\mathcal{T}_{77} = 0, \quad \mathcal{T}_{m} = 0$$

$$\mathcal{E}_{nn} = \frac{1}{E} \left[ \mathcal{T}_{nn} - \mathcal{D} \mathcal{T}_{ry} \right] = \frac{1}{E} \times \frac{T}{a}$$

$$\mathcal{T}_{nn} = \frac{1}{E} \left[ \mathcal{T}_{nn} - \mathcal{D} \mathcal{T}_{ry} \right] = \frac{1}{E} \times \frac{T}{a}$$

$$\mathcal{E}_{yy} = \frac{1}{E} \left[ \mathcal{O}_{yy} - \mathcal{N}_{nn} \right] = -\frac{\lambda}{E} \mathcal{E}_{a}$$

u, V 生

$$\begin{aligned}
\varphi &= Ay^3 \rightarrow fiq = 6Ay \\
\nabla_{xx} &= \frac{50}{50x} = 6Ay \\
\nabla_{yy} &= \frac{50}{50x} = 0
\end{aligned}$$

$$\nabla_{yy} &= \frac{50}{50x} = 0$$

$$\nabla_{yy} &= -\frac{50}{50x} = 0$$