

# 2D ELASTICITY\*

## 1 Plane stress

The salient features of a plane stress situation are:

- Domain bounded by two parallel planes
- Distance between two planes is small compared to other dimensions
- When referred to a rectangular Cartesian coordinate system, it is usual to take the two planes to be represented by  $z = \pm h$  such that the *very small* distance between the two planes is  $2h$ , and the  $x - y$  plane (denoting the mid-surface) is used to describe the problem.
- The two planes  $z = h$  and  $z = -h$  are stress-free so that  $\sigma_{zz} = \sigma_{xz} = \sigma_{yz} = 0$  on each face.
- It is expected that there will be very little variation in  $\sigma_{zz}$ ,  $\sigma_{xz}$ , and  $\sigma_{yz}$  through the thickness; hence, they are approximately taken as zero throughout the entire domain.
- Again because of the very small thickness, the non-zero stress components will have little variation with  $z$ ; they are approximately taken to be *independent* of  $z$ . Thus,

$$\sigma_{xx} \equiv \sigma_{xx}(x, y), \sigma_{yy} \equiv \sigma_{yy}(x, y), \sigma_{xy} \equiv \sigma_{xy}(x, y).$$

- There can be no body forces in the  $z$ -direction; this follows immediately from the  $z$ -component of the mechanical equilibrium equation.

From constitutive equation of a linear, elastic, isotropic solid, we have

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for the plane stress situation:

$$\varepsilon_{xx} = \frac{1}{E} (\sigma_{xx} - \nu \sigma_{yy}), \quad (1a)$$

$$\varepsilon_{yy} = \frac{1}{E} (\sigma_{yy} - \nu \sigma_{xx}), \quad (1b)$$

$$\varepsilon_{zz} = -\frac{\nu}{E} (\sigma_{xx} + \sigma_{yy}), \quad (1c)$$

$$\varepsilon_{xy} = \frac{1 + \nu}{E} \sigma_{xy}, \quad (1d)$$

$$\varepsilon_{yz} = 0, \quad (1e)$$

$$\varepsilon_{zx} = 0. \quad (1f)$$

Adding (1a) and (1b) and substituting in (1c), we have

$$\varepsilon_{zz} = -\frac{\nu}{1 - \nu} (\varepsilon_{xx} + \varepsilon_{yy}). \quad (2)$$

**NOTE:**

- Even though  $\sigma_{zz} = \sigma_{xz} = \sigma_{yz} = 0$ , we still have  $\varepsilon_{zz} \neq 0$ .
- All strains are independent of  $z$ .

Now, consider the compatibility equations<sup>†</sup>:

$$\frac{\partial^2 \varepsilon_{xx}}{\partial y^2} + \frac{\partial^2 \varepsilon_{yy}}{\partial x^2} = 2 \frac{\partial^2 \varepsilon_{xy}}{\partial x \partial y}, \quad (3a)$$

$$\frac{\partial^2 \varepsilon_{yy}}{\partial z^2} + \frac{\partial^2 \varepsilon_{zz}}{\partial y^2} = 2 \frac{\partial^2 \varepsilon_{yz}}{\partial y \partial z}, \quad (3b)$$

$$\frac{\partial^2 \varepsilon_{zz}}{\partial x^2} + \frac{\partial^2 \varepsilon_{xx}}{\partial z^2} = 2 \frac{\partial^2 \varepsilon_{zx}}{\partial z \partial x}, \quad (3c)$$

$$\frac{\partial^2 \varepsilon_{xx}}{\partial y \partial z} = \frac{\partial}{\partial x} \left( -\frac{\partial \varepsilon_{yz}}{\partial x} + \frac{\partial \varepsilon_{zx}}{\partial y} + \frac{\partial \varepsilon_{xy}}{\partial z} \right), \quad (3d)$$

$$\frac{\partial^2 \varepsilon_{yy}}{\partial z \partial x} = \frac{\partial}{\partial y} \left( -\frac{\partial \varepsilon_{zx}}{\partial y} + \frac{\partial \varepsilon_{xy}}{\partial z} + \frac{\partial \varepsilon_{yz}}{\partial x} \right), \quad (3e)$$

$$\frac{\partial^2 \varepsilon_{zz}}{\partial x \partial y} = \frac{\partial}{\partial z} \left( -\frac{\partial \varepsilon_{xy}}{\partial z} + \frac{\partial \varepsilon_{yz}}{\partial x} + \frac{\partial \varepsilon_{zx}}{\partial y} \right). \quad (3f)$$

<sup>†</sup>Refer to Problem Sheet 1 on “Kinematics”.

The only compatibility equation that is considered is (3a). The other three compatibility equations involving  $\varepsilon_{zz}$  are neglected.

Now, using (1a) and (1b) in (3a), we have, after rearranging

$$\left(-\nu \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2}\right) \sigma_{xx} + \left(\frac{\partial^2}{\partial x^2} - \nu \frac{\partial^2}{\partial y^2}\right) \sigma_{yy} = 2(1 + \nu) \frac{\partial^2 \sigma_{xy}}{\partial x \partial y}. \quad (4)$$

Adding and subtracting  $\frac{\partial^2 \sigma_{xx}}{\partial x^2}$  and  $\frac{\partial^2 \sigma_{yy}}{\partial y^2}$ , we have

$$-(1 + \nu) \left( \frac{\partial^2 \sigma_{xx}}{\partial x^2} + \frac{\partial^2 \sigma_{yy}}{\partial y^2} \right) + \nabla^2 (\sigma_{xx} + \sigma_{yy}) = 2(1 + \nu) \frac{\partial^2 \sigma_{xy}}{\partial x \partial y}. \quad (5)$$

Consider the equilibrium equations

$$\frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \sigma_{xy}}{\partial y} + F_x = 0, \quad (6a)$$

$$\frac{\partial \sigma_{xy}}{\partial x} + \frac{\partial \sigma_{yy}}{\partial y} + F_y = 0, \quad (6b)$$

Differentiating the first of the preceding equations with respect to  $x$  and the second with respect to  $y$ , we have

$$\frac{\partial^2 \sigma_{xx}}{\partial x^2} + \frac{\partial^2 \sigma_{xy}}{\partial x \partial y} = -\frac{\partial F_x}{\partial x}, \quad (7a)$$

$$\frac{\partial^2 \sigma_{xy}}{\partial y \partial x} + \frac{\partial^2 \sigma_{yy}}{\partial y^2} = -\frac{\partial F_y}{\partial y}. \quad (7b)$$

Adding these two equations, we obtain

$$\frac{\partial^2 \sigma_{xx}}{\partial x^2} + \frac{\partial^2 \sigma_{yy}}{\partial y^2} + 2 \frac{\partial^2 \sigma_{xy}}{\partial x \partial y} = -\left( \frac{\partial F_x}{\partial x} + \frac{\partial F_y}{\partial y} \right). \quad (8)$$

Substituting (8) in (5), we have

$$\nabla^2 (\sigma_{xx} + \sigma_{yy}) = -(1 + \nu) \left( \frac{\partial F_x}{\partial x} + \frac{\partial F_y}{\partial y} \right). \quad (9)$$

We consider the equilibrium equations agains but assume the body forces to be conservative in nature so that they are expressed as the gradient of a scalar potential, i.e.  $F_x = -\frac{\partial V}{\partial x}$  and  $F_y = -\frac{\partial V}{\partial y}$ , so that

$$\frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \sigma_{xy}}{\partial y} - \frac{\partial V}{\partial x} = 0, \quad (10a)$$

$$\frac{\partial \sigma_{xy}}{\partial x} + \frac{\partial \sigma_{yy}}{\partial y} - \frac{\partial V}{\partial y} = 0. \quad (10b)$$

We define the following:

$$\sigma_{xx} - V = \frac{\partial^2 \varphi}{\partial y^2}, \quad (11a)$$

$$\sigma_{yy} - V = \frac{\partial^2 \varphi}{\partial x^2}, \quad (11b)$$

$$\sigma_{xy} = -\frac{\partial^2 \varphi}{\partial x \partial y}, \quad (11c)$$

so that (10a) and (10b) are satisfied identically.

Using the expressions of  $\sigma_{xx}$  and  $\sigma_{yy}$  in Eq. (9), we have

$$\begin{aligned} & \left( \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right) \left( V + \frac{\partial^2 \varphi}{\partial y^2} \right) + \left( \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right) \left( V + \frac{\partial^2 \varphi}{\partial x^2} \right) = (1 + \nu) \left( \frac{\partial^2 V}{\partial x^2} + \frac{\partial^2 V}{\partial y^2} \right), \\ \text{or, } & 2\nabla^2 V + \nabla^2(\nabla^2 \varphi) = (1 + \nu)\nabla^2 V, \\ \text{or, } & \nabla^4 \varphi = -(1 - \nu)\nabla^2 V \end{aligned} \quad (12)$$

Note that  $\nabla^4$  is referred to as the biharmonic operator.

If the body forces vanish or if  $\nabla^2 V = 0$  then we have

$$\nabla^4 \varphi = 0. \quad (13)$$

This equation is referred to as the biharmonic equation, and its solutions are referred to as the biharmonic solutions.

## 2 Plane Strain

Consider an infinitely long cylindrical (prismatic) body

- If body forces and tractions on the lateral boundaries are independent of the longitudinal axis variable,  $z$ , and have no  $z$ -component then the deformation field can be taken as

$$u \equiv u(x, y), \quad v \equiv v(x, y)$$

This deformation is referred to as a state of plane strain in the  $x - y$  plane.

- All cross sections will have identical displacements and thus the 3D problem is reduced to a 2D problem.

Considering the preceding points, we have

$$\begin{aligned} \varepsilon_{xx} &= \frac{\partial u}{\partial x}, \quad \varepsilon_{yy} = \frac{\partial v}{\partial y}, \quad \varepsilon_{xy} = \frac{1}{2} \left( \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right), \\ \varepsilon_{zz} &= \varepsilon_{zx} = \varepsilon_{yz} = 0. \end{aligned}$$

The only compatibility equation that does not reduce to a  $0 = 0$  form is

$$\frac{\partial^2 \varepsilon_{xx}}{\partial y^2} + \frac{\partial^2 \varepsilon_{yy}}{\partial x^2} = 2 \frac{\partial^2 \varepsilon_{xy}}{\partial x \partial y}. \quad (14)$$

Considering the constitutive equation for a linear, elastic, isotropic material we have

$$\varepsilon_{xx} = \frac{1}{E} \left[ \sigma_{xx} - \nu (\sigma_{yy} + \sigma_{zz}) \right], \quad (15a)$$

$$\varepsilon_{yy} = \frac{1}{E} \left[ \sigma_{yy} - \nu (\sigma_{zz} + \sigma_{xx}) \right], \quad (15b)$$

$$\varepsilon_{zz} = \frac{1}{E} \left[ \sigma_{zz} - \nu (\sigma_{xx} + \sigma_{yy}) \right] \implies \sigma_{zz} = \nu (\sigma_{xx} + \sigma_{yy}), \quad (15c)$$

$$\varepsilon_{xy} = \frac{1 + \nu}{E} \sigma_{xy}, \quad (15d)$$

$$\sigma_{yz} = \sigma_{zx} = 0 \quad (\text{Since } \varepsilon_{yz} = \varepsilon_{zx} = 0) \quad (15e)$$

Note that unlike the plane stress case, in the plane strain case we have  $\sigma_{zz} \neq 0$ .

Substituting the expression of  $\sigma_{zz}$  in the expressions for  $\varepsilon_{xx}$  and  $\varepsilon_{yy}$ , we have

$$\varepsilon_{xx} = \frac{1 + \nu}{E} [(1 - \nu)\sigma_{xx} - \nu\sigma_{yy}], \quad (16a)$$

$$\varepsilon_{yy} = \frac{1 + \nu}{E} [(1 - \nu)\sigma_{yy} - \nu\sigma_{xx}]. \quad (16b)$$

We next use these expressions for  $\varepsilon_{xx}$  and  $\varepsilon_{yy}$  (from Eq. (16)(a) and (b)) as well as for  $\varepsilon_{xy}$  (from Eq. (15)(c)) in the compatibility equation, Eq. (14), to obtain

$$\frac{1 + \nu}{E} \frac{\partial^2}{\partial y^2} [(1 - \nu)\sigma_{xx} - \nu\sigma_{yy}] + \frac{1 + \nu}{E} \frac{\partial^2}{\partial x^2} [(1 - \nu)\sigma_{yy} - \nu\sigma_{xx}] = 2 \frac{1 + \nu}{E} \frac{\partial^2 \sigma_{xy}}{\partial x \partial y}, \quad (17)$$

$$\text{or, } (1 - \nu)\nabla^2 (\sigma_{xx} + \sigma_{yy}) - \frac{\partial^2 \sigma_{xx}}{\partial x^2} - \frac{\partial^2 \sigma_{yy}}{\partial y^2} = 2 \frac{\partial^2 \sigma_{xy}}{\partial x \partial y}. \quad (18)$$

Considering the equilibrium equations, we have

$$\frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \sigma_{xy}}{\partial y} + F_x = 0 \implies \frac{\partial^2 \sigma_{xx}}{\partial x^2} + \frac{\partial^2 \sigma_{xy}}{\partial x \partial y} + \frac{\partial f_x}{\partial x} = 0, \quad (19a)$$

$$\frac{\partial \sigma_{xy}}{\partial x} + \frac{\partial \sigma_{yy}}{\partial y} + F_y = 0 \implies \frac{\partial^2 \sigma_{xy}}{\partial x \partial y} + \frac{\partial^2 \sigma_{yy}}{\partial y^2} + \frac{\partial f_y}{\partial y} = 0. \quad (19b)$$

Partially differentiating the first of the preceding equations with respect to  $x$  and the second with respect to  $y$ , and adding them, we obtain

$$\frac{\partial^2 \sigma_{xx}}{\partial x^2} + \frac{\partial^2 \sigma_{yy}}{\partial y^2} + 2 \frac{\partial^2 \sigma_{xy}}{\partial x \partial y} = - \left( \frac{\partial f_x}{\partial x} + \frac{\partial f_y}{\partial y} \right). \quad (20)$$

Using Eq. (20) in Eq. (18), we obtain

$$(1 - \nu)\nabla^2 (\sigma_{xx} + \sigma_{yy}) = - \left( \frac{\partial f_x}{\partial x} + \frac{\partial f_y}{\partial y} \right). \quad (21)$$

Proceeding similarly as in the plane stress case we consider a conservative body force per unit volume, we set

$$\sigma_{xx} = \frac{\partial^2 \varphi}{\partial y^2} + V, \quad (22a)$$

$$\sigma_{yy} = \frac{\partial^2 \varphi}{\partial x^2} + V, \quad (22b)$$

$$\sigma_{xy} = -\frac{\partial^2 \varphi}{\partial x \partial y}, \quad (22c)$$

where  $V$  is a scalar potential such that  $f_x = -\frac{\partial V}{\partial x}$  and  $f_y = -\frac{\partial V}{\partial y}$ .

Using these expressions in Eq. (21), we have

$$(1 - \nu) \nabla^2 \left( \frac{\partial^2 \varphi}{\partial y^2} + V + \frac{\partial^2 \varphi}{\partial x^2} + V \right) = \nabla^2 V,$$

$$\text{or, } \nabla^4 \varphi = -\frac{1 - 2\nu}{1 - \nu} \nabla^2 V. \quad (23)$$

Again, as in the plane stress case, if the body forces vanish or if  $\nabla^2 V = 0$  then we have

$$\nabla^4 \varphi = 0. \quad (24)$$

Summary for plane stress and plane strain cases:

$$\text{Plane stress: } \nabla^4 \varphi = -(1 - \nu) \nabla^2 V, \quad (25)$$

$$\text{Plane strain: } \nabla^4 \varphi = -\frac{1 - 2\nu}{1 - \nu} \nabla^2 V. \quad (26)$$