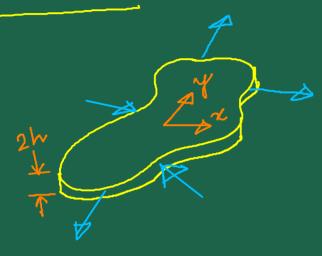
2D Elasticity

Plane Stross



- # Domain bounded by two parallel planes
- # Distance between these two planes is very small compared to other dimensions
- # The two planes are at $Z = \pm h$
- # The two planes are stress-free: $\mathcal{J}_{zz} = \mathcal{J}_{zz} = \mathcal{J}_{zz} = \mathcal{J}_{zz}$
- # There is very little variation in T₂₂, T_{2n}, T₇ through the thickness; in fact these will be approximated to be zero

Because of the very small thickness, the non-zero components will have very little variation in the z-direction

$$\mathcal{T}_{nn} = \mathcal{T}_{nn}(x,y); \quad \mathcal{T}_{yy} = \mathcal{T}_{yy}(x,y); \quad \mathcal{T}_{ny} = \mathcal{T}_{ny}(x,y)$$

- # In order to have these stresses to be independent of z,we must not have any body forces or tractions in the z-direction
- # Non-zero body forces or tractions must be independent of z

$$\mathcal{E}_{nn} = \frac{1}{E} \left[\mathcal{T}_{nn} - \mathcal{S}(\mathcal{T}_{77} + \mathcal{T}_{22}) \right] - \mathcal{D}$$

$$\mathcal{E}_{yy} = \frac{1}{E} \left[\mathcal{T}_{yy} - \mathcal{S}(\mathcal{T}_{nn} + \mathcal{T}_{22}) \right] - \mathcal{D}$$

$$\mathcal{E}_{zz} = \frac{1}{E} \left[\mathcal{T}_{zz} - \mathcal{S}(\mathcal{T}_{nn} + \mathcal{T}_{ry}) \right] - \mathcal{D}$$

$$\mathcal{E}_{zz} = \frac{1}{E} \left[\mathcal{T}_{zz} - \mathcal{S}(\mathcal{T}_{nn} + \mathcal{T}_{ry}) \right] - \mathcal{D}$$

$$\mathcal{E}_{yz} = \frac{1}{24} \mathcal{T}_{ry} = \frac{1+\mathcal{D}}{E} \mathcal{T}_{ry} - \mathcal{D}$$

$$\mathcal{E}_{yz} = \frac{1}{24} \mathcal{T}_{ry} = \mathcal{D}$$

 $\Sigma_{ZX} = \frac{1}{24} \mathcal{I}_{ZX} = 0$ All strains are independent of Z

strus eyb. egns

$$\frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \sigma_{xy}}{\partial y} + \frac{\partial \sigma_{xx}}{\partial z} = 0$$

Airy Stress Function

 $\int_{xx} = \frac{39}{3y^2}, \quad Gyy = \frac{39}{3x^2}, \quad Gyy = -\frac{39}{3x^3y}$

> Suls. in stross ents. agris -> identically satisfies them!

But we must be careful in choosing of. For some arbitrary (50) choice of of it may turn out that the strains are incompatible!

-> This is ensured by articly including in the mathematical framework of the Biry Gress Function, the compatibility equis.

$$\frac{\partial \mathcal{E}_{11}}{\partial y} + \frac{\partial \mathcal{E}_{12}}{\partial x^{2}} = 2 \frac{\partial \mathcal{E}_{12}}{\partial x^{2}}$$

$$\frac{\partial \mathcal{E}_{22}}{\partial z^{2}} + \frac{\partial \mathcal{E}_{22}}{\partial z^{2}} = 2 \frac{\partial \mathcal{E}_{22}}{\partial x^{2}} \Rightarrow \frac{\partial \mathcal{E}_{22}}{\partial y^{2}} = 0$$

$$\frac{\partial \mathcal{E}_{22}}{\partial x^{2}} + \frac{\partial \mathcal{E}_{12}}{\partial z^{2}} = 2 \frac{\partial \mathcal{E}_{21}}{\partial x^{2}} \Rightarrow \frac{\partial \mathcal{E}_{22}}{\partial x^{2}} = 0$$

$$\frac{\partial \mathcal{E}_{22}}{\partial x^{2}} + \frac{\partial \mathcal{E}_{12}}{\partial z^{2}} = 2 \frac{\partial \mathcal{E}_{21}}{\partial x^{2}} \Rightarrow \frac{\partial \mathcal{E}_{22}}{\partial x^{2}} = 0$$

$$\frac{\partial \mathcal{E}_{12}}{\partial x^{2}} = \frac{\partial}{\partial x} \left(-\frac{\partial \mathcal{E}_{12}}{\partial x} + \frac{\partial \mathcal{E}_{12}}{\partial y^{2}} + \frac{\partial \mathcal{E}_{12}}{\partial x^{2}} \right) \Rightarrow 0 = 0$$

$$\frac{\partial \mathcal{E}_{12}}{\partial x^{2}} = \frac{\partial}{\partial x} \left(\frac{\partial \mathcal{E}_{12}}{\partial x} - \frac{\partial \mathcal{E}_{21}}{\partial y^{2}} + \frac{\partial \mathcal{E}_{12}}{\partial z^{2}} \right) \Rightarrow 0 = 0$$

$$\frac{\partial \mathcal{E}_{22}}{\partial x^{2}} = \frac{\partial}{\partial x} \left(\frac{\partial \mathcal{E}_{12}}{\partial x} + \frac{\partial \mathcal{E}_{12}}{\partial y^{2}} - \frac{\partial \mathcal{E}_{12}}{\partial z^{2}} \right) \Rightarrow 0 = 0$$

$$\frac{\partial \mathcal{E}_{22}}{\partial x^{2}} = \frac{\partial}{\partial x} \left(\frac{\partial \mathcal{E}_{12}}{\partial x} + \frac{\partial \mathcal{E}_{22}}{\partial y^{2}} - \frac{\partial \mathcal{E}_{12}}{\partial z^{2}} \right) \Rightarrow 0 = 0$$

$$\frac{\partial \mathcal{E}_{22}}{\partial x^{2}} = \frac{\partial}{\partial x} \left(\frac{\partial \mathcal{E}_{12}}{\partial x} + \frac{\partial \mathcal{E}_{22}}{\partial y^{2}} - \frac{\partial \mathcal{E}_{12}}{\partial z^{2}} \right) \Rightarrow 0 = 0$$

$$\frac{\tilde{\partial} \mathcal{E}_{xx}}{\partial y^{L}} + \frac{\tilde{\partial} \mathcal{E}_{yy}}{\partial x^{N}} = 2 \frac{\tilde{\partial} \mathcal{E}_{xy}}{\partial x^{N}} - (5)$$

$$Varg (1), (2) & (3) in (5):$$

$$\frac{1}{E} \frac{\tilde{\partial}}{\partial y^{L}} (\mathcal{I}_{xx} - 5 \mathcal{E}_{yy}) + \frac{1}{E} \frac{\tilde{\partial}}{\partial x^{L}} (\mathcal{I}_{yy} - 5 \mathcal{E}_{xx}) = 2 \frac{1+\tilde{\partial}}{E} \frac{\tilde{\partial}}{\partial x^{N}} (\mathcal{I}_{xy})$$

$$\Rightarrow (-1) \frac{\tilde{\partial}}{\partial x^{L}} + \frac{\tilde{\partial}}{\partial y^{L}} (\mathcal{I}_{xx} + (\frac{\tilde{\partial}}{\partial x^{L}} - \frac{\tilde{\partial}}{\partial y^{L}}) \mathcal{E}_{xx} + (\frac{\tilde{\partial}}{\partial x^{L}} + \frac{\tilde{\partial}}{\partial y^{L}}) \mathcal{E}_{xx} + (\frac{\tilde{\partial}}{\partial$$

$$\frac{\partial G_{xx}}{\partial x} + \frac{\partial G_{xy}}{\partial y} + F_{x} = 0 \Rightarrow \frac{\partial G_{xx}}{\partial x^{2}} + \frac{\partial G_{xy}}{\partial x^{2}} = -\frac{\partial F_{x}}{\partial x} - 0$$

$$\frac{\partial G_{xy}}{\partial x} + \frac{\partial G_{yy}}{\partial y} + F_{y} = 0 \Rightarrow \frac{\partial G_{xy}}{\partial y^{2}} + \frac{\partial G_{yy}}{\partial y^{2}} = -\frac{\partial F_{y}}{\partial y} - 8$$

$$\Rightarrow \frac{\partial G_{xx}}{\partial x^{2}} + \frac{\partial G_{yy}}{\partial y^{2}} + 2\frac{\partial G_{xy}}{\partial x^{2}} = -\frac{\partial F_{x}}{\partial y} - 9$$

$$\frac{\partial G_{xx}}{\partial x^{2}} + \frac{\partial G_{yy}}{\partial y^{2}} + 2\frac{\partial G_{xy}}{\partial x^{2}} = -\frac{\partial F_{x}}{\partial y} - 9$$

$$\frac{\partial G_{xx}}{\partial x^{2}} + \frac{\partial G_{xy}}{\partial y^{2}} + 2\frac{\partial G_{xy}}{\partial x^{2}} = -\frac{\partial F_{x}}{\partial y} - 9$$

$$\frac{\partial G_{xx}}{\partial x^{2}} + \frac{\partial G_{xy}}{\partial x^{2}} + \frac{\partial G_{xy}}{\partial x^{2}} + \frac{\partial G_{xy}}{\partial y^{2}} + \frac{\partial G_{xy}}{\partial y^{2}} = -\frac{\partial F_{x}}{\partial y} - 9$$

$$\frac{\partial G_{xx}}{\partial x^{2}} + \frac{\partial G_{xy}}{\partial x^{2}} + \frac{\partial G_{xy}}{\partial x^{2}} + \frac{\partial G_{xy}}{\partial y^{2}} + \frac{\partial G_{xy}}{\partial y^{2}} = -\frac{\partial F_{x}}{\partial y} - 9$$

$$\frac{\partial G_{xx}}{\partial x^{2}} + \frac{\partial G_{xy}}{\partial y^{2}} + \frac{\partial G_{xy}}{\partial y$$

7

We consider body forces that are conservative in rature $F_n = -\frac{\partial V}{\partial n}$ $_2$ $F_y = -\frac{\partial V}{\partial y}$ $\left[\vec{F} = -\nabla V\right]$ $\frac{\partial \mathcal{L}_{xx}}{\partial x} + \frac{\partial \mathcal{L}_{ny}}{\partial y} - \frac{\partial \mathcal{V}}{\partial x} = 0 \Rightarrow \frac{\partial}{\partial x} (\mathcal{L}_{nn} - \mathcal{V}) + \frac{\partial \mathcal{L}_{ny}}{\partial y} = 0 - 0$ 30 m + 30 m = 0 = 20 = 20 mm + 2 (Cyy-V) = 0-12 $G_{nn}-V=\frac{\partial Q}{\partial y^2}$, $G_{yy}-V=\frac{\partial Q}{\partial n^2}$, $G_{ny}=-\frac{\partial Q}{\partial n^2}$

 $(D) \rightarrow \nabla (T_{n} + C_{yy}) = (1+i) \frac{\partial V}{\partial n^{2}} + \frac{\partial V}{\partial y^{2}}$

$$\frac{\partial^{2}(v+\frac{\partial^{2}\phi}{\partial y^{2}}+v+\frac{\partial^{2}\phi}{\partial y^{2}})=(1+v)\frac{\partial^{2}v}{\partial v}$$

$$\Rightarrow 2\frac{\partial^{2}v}{\partial y}+\frac{\partial^{2}(\sqrt{2}\phi)}{(1-v)}=(1+v)\frac{\partial^{2}v}{\partial v}$$

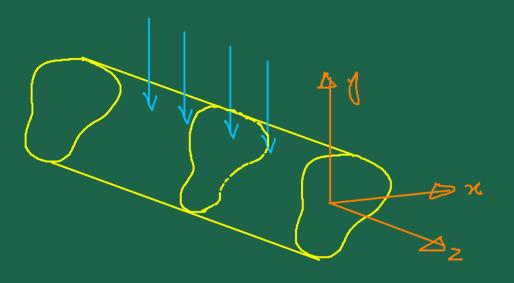
$$\Rightarrow \frac{\partial^{2}\phi}{\partial y}=-(1-v)\frac{\partial^{2}v}{\partial v}-(13)$$

$$\Rightarrow \frac{\partial^{2}\phi}{\partial v}=-(1-v)\frac{\partial^{2}v}{\partial v}-(13)$$

$$\Rightarrow \frac{\partial^{2}\phi}{\partial v}=-(1-v)\frac{\partial^{2}\phi}{\partial v}$$

$$\Rightarrow \frac{\partial^{2}\phi}{\partial v}=-(1-v)$$

Plane Strain



If body forces and tractions are uniform along 2 and do not have any 2-component, then $u \equiv u(x,y)$, $v \equiv v(x,y)$, $w \equiv 0$

$$\xi_{XX} = \frac{3\sqrt{3}}{3\sqrt{3}}$$

$$\xi_{YY} = \frac{3\sqrt{3}}{3\sqrt{3}}$$

$$\xi_{YY} = \frac{1}{2} \left(\frac{3\sqrt{3}}{3\sqrt{3}} + \frac{3\sqrt{3}}{3\sqrt{3}} \right)$$

$$\xi_{ZX} = \frac{1}{2} \left(\frac{3\sqrt{3}}{3\sqrt{3}} + \frac{3\sqrt{3}}{3\sqrt{2}} \right) = 0$$

$$\xi_{YZ} = \frac{1}{2} \left(\frac{3\sqrt{3}}{3\sqrt{3}} + \frac{3\sqrt{3}}{3\sqrt{2}} \right) = 0$$

$$\mathcal{E}_{XA} = \frac{1}{E} \left[\mathcal{C}_{XA} - \mathcal{V} \left(\mathcal{C}_{YY} + \mathcal{C}_{ZZ} \right) \right] \Rightarrow \mathcal{E}_{XA} = \frac{1}{E} \left[\mathcal{C}_{XA} - \mathcal{V} \left(\mathcal{C}_{YY} + \mathcal{V}_{XA} + \mathcal{C}_{YY} \right) \right] \\
= \frac{1}{E} \left[\mathcal{C}_{ZY} - \mathcal{V} \left(\mathcal{C}_{XA} + \mathcal{C}_{YY} \right) \right] \\
= \frac{1}{E} \left[(-\mathcal{V}) \mathcal{C}_{XA} - \mathcal{V} \left(\mathcal{C}_{YY} + \mathcal{V}_{YY} \right) \right] \\
= \frac{1}{E} \left[(-\mathcal{V}) \mathcal{C}_{XA} - \mathcal{V} \left(\mathcal{C}_{YY} + \mathcal{V}_{YY} \right) \right] \\
= \frac{1}{E} \left[(-\mathcal{V}) \mathcal{C}_{XA} - \mathcal{V} \left(\mathcal{C}_{YY} + \mathcal{V}_{YY} \right) \right] \\
= \frac{1}{E} \left[(-\mathcal{V}) \mathcal{C}_{XA} - \mathcal{V}_{YY} \right] \\
= \frac{1}{E} \left[(-\mathcal{V}) \mathcal{C}_{YY} - \mathcal{V}_{XA} \right] \\
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= \frac{1}{E} \left[(-\mathcal{V}) \mathcal{C}_{YY} - \mathcal{V}_{YY} \right] \\
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= \frac{1}{E} \left[(-\mathcal{V}) \mathcal{C}_{YY} - \mathcal{V}_{YY} \right] \\
= \frac{1}{E} \left[(-\mathcal{V}) \mathcal{C}_{YY} - \mathcal{V}_{YY} \right] \\
= \frac{1}{E} \left[(-\mathcal{V}) \mathcal{C}$$

$$\frac{2\pi}{2\pi} = \frac{1+\sqrt{2\pi}}{E} \left[(1-\sqrt{2}) C_{\gamma\gamma} - \sqrt{2\pi} C_{\gamma\gamma} - \sqrt{2\pi} C_{\gamma\gamma} \right] - \left[2 \right]$$

$$\frac{2C_{\gamma\gamma}}{2\pi} + \frac{2C_{\gamma\gamma}}{2\gamma} + \frac{2C_{\gamma\gamma}}{2\gamma} = 0$$

$$\frac{2C_{\gamma\gamma}}{2\pi} + \frac{2C_{\gamma\gamma}}{2\gamma} + \frac{2C_{\gamma\gamma}}{2\gamma} = 0$$

$$\frac{2C_{\gamma\gamma}}{2\pi} + \frac{2C_{\gamma\gamma}}{2\gamma} + \frac{2C_{\gamma\gamma}}{2\gamma} = 0$$

 $=\frac{1}{F}\left[\left(-5\right)\nabla_{xx}-5\left(1+1\right)\nabla_{yy}\right]$

 $=\frac{1+\sqrt{1-1}}{1-1}\left[\left(1-\sqrt{1-1}\right)\sqrt{1-1}\sqrt{1-1}\right]$

$$\frac{\partial \mathcal{E}_{AA}}{\partial y^{2}} + \frac{\partial \mathcal{E}_{yy}}{\partial n^{2}} = 2 \frac{\partial \mathcal{E}_{my}}{\partial n^{2}y} - 5$$

$$\Rightarrow \frac{1+\sqrt{3}}{E} \frac{\partial}{\partial y^{2}} \left[\left(-\frac{1}{2} \right) \sigma_{nn} - \frac{1}{2} \sigma_{yy} \right] + \frac{1+\sqrt{3}}{E} \frac{\partial}{\partial x^{2}} \left[\left(-\frac{1}{2} \right) \sigma_{yy} - \frac{1}{2} \sigma_{ny} \right] = 2 \frac{1+\sqrt{3}}{E} \frac{\partial^{2} \sigma_{ny}}{\partial n^{2}y}$$

$$\Rightarrow \left(1-\sqrt{3} \frac{\partial^{2} \sigma_{ny}}{\partial n^{2}} + \frac{\partial^{2} \sigma_{yy}}{\partial y^{2}} \right) \left(-\frac{1}{2} \frac{\partial^{2} \sigma_{yy}}{\partial n^{2}} + \frac{\partial^{2} \sigma_{yy}}{\partial y^{2}} \right) \left(-\frac{1}{2} \frac{\partial^{2} \sigma_{yy}}{\partial n^{2}} \right) \left(-\frac{1}{2} \frac{\partial^{2} \sigma_{yy}}{\partial n^{2}} \right) \left(-\frac{1}{2} \frac{\partial^{2} \sigma_{yy}}{\partial n^{2}} \right) = 2 \frac{\partial^{2} \sigma_{ny}}{\partial n^{2}y} - 6$$

$$\Rightarrow \left(1-\sqrt{3} \frac{\partial^{2} \sigma_{ny}}{\partial n^{2}} - \left(1-\sqrt{3} \frac{\partial^{2} \sigma_{yy}}{\partial n^{2}} \right) - \frac{\partial^{2} \sigma_{ny}}{\partial n^{2}y} \right) \left(-\frac{\partial^{2} \sigma_{ny}}{\partial n^{2}} - \frac{\partial^{2} \sigma_{ny}}{\partial n^{2}} \right) \left(-\frac{\partial^{2} \sigma_{ny}}{\partial n^{2}}$$

$$\frac{\partial G_{nn}}{\partial L} + \frac{\partial G_{ny}}{\partial y} + F_{n} = D \Rightarrow \frac{\partial G_{nx}}{\partial x^{2}} + \frac{\partial G_{ny}}{\partial x^{2}} = -\frac{\partial F_{n}}{\partial x} - D$$

$$\frac{\partial G_{ny}}{\partial x} + \frac{\partial G_{ny}}{\partial y} + F_{y} = D \Rightarrow \frac{\partial G_{ny}}{\partial y^{2}} + \frac{\partial G_{ny}}{\partial y^{2}} = -\frac{\partial F_{y}}{\partial y} - B$$

$$\Rightarrow \frac{\partial G_{nn}}{\partial x^{2}} + \frac{\partial G_{yy}}{\partial y} + 2\frac{\partial G_{ny}}{\partial x^{2}} = -\frac{\partial F_{y}}{\partial y} - D$$

$$\frac{\partial G_{nn}}{\partial x^{2}} + \frac{\partial G_{yy}}{\partial y^{2}} + 2\frac{\partial G_{ny}}{\partial x^{2}} = -\frac{\partial F_{y}}{\partial x} - D$$

$$\frac{\partial G_{nn}}{\partial x^{2}} + \frac{\partial G_{yy}}{\partial y^{2}} + 2\frac{\partial G_{ny}}{\partial x^{2}} - \frac{\partial F_{y}}{\partial x} - D$$

$$\frac{\partial G_{nn}}{\partial x^{2}} + \frac{\partial G_{ny}}{\partial y^{2}} + 2\frac{\partial G_{ny}}{\partial x^{2}} - \frac{\partial G_{ny}}{\partial x} - D$$

$$\frac{\partial G_{nn}}{\partial x^{2}} + \frac{\partial G_{ny}}{\partial x^{2}} - \frac{\partial G_{ny}}{\partial x^{2}} - \frac{\partial G_{ny}}{\partial x^{2}} - D$$

$$\frac{\partial G_{nn}}{\partial x^{2}} + \frac{\partial G_{ny}}{\partial x^{2}} - \frac{\partial G_{ny}}{\partial x^{2}} - \frac{\partial G_{ny}}{\partial x^{2}} - D$$

$$\frac{\partial G_{nn}}{\partial x^{2}} + \frac{\partial G_{ny}}{\partial y^{2}} - \frac{\partial G_{ny}}{\partial x^{2}} - \frac{\partial G_{ny}}{\partial x^{2}} - D$$

$$\frac{\partial G_{nn}}{\partial x^{2}} + \frac{\partial G_{ny}}{\partial x^{2}} - \frac{\partial G_{ny}}{\partial x^{2}} - \frac{\partial G_{ny}}{\partial x^{2}} - D$$

$$\frac{\partial G_{nn}}{\partial x^{2}} + \frac{\partial G_{ny}}{\partial x^{2}} - \frac{\partial G_{ny}}{\partial x^{2}} - \frac{\partial G_{ny}}{\partial x^{2}} - \frac{\partial G_{ny}}{\partial x^{2}} - D$$

$$\frac{\partial G_{nn}}{\partial x^{2}} + \frac{\partial G_{ny}}{\partial x^{2}} - \frac{\partial G_{ny}}{\partial x^{2}} - \frac{\partial G_{ny}}{\partial x^{2}} - \frac{\partial G_{ny}}{\partial x^{2}} - D$$

$$\frac{\partial G_{ny}}{\partial x^{2}} + \frac{\partial G_{ny}}{\partial x^{2}} - \frac{\partial G_{ny}$$

Consider the stress eglo coms again but with conservative body forces

$$\frac{\partial \mathcal{T}_{nn}}{\partial x} + \frac{\partial \mathcal{T}_{ny}}{\partial y} - \frac{\partial \mathcal{V}}{\partial x} = 0 \Rightarrow \frac{\partial}{\partial x} \left(\mathcal{T}_{nn} - \mathcal{V} \right) + \frac{\partial \mathcal{T}_{ny}}{\partial y} = 0$$

$$\frac{\partial \nabla_{xy}}{\partial x} + \frac{\partial C_{yy}}{\partial y} - \frac{\partial V}{\partial y} = 0 \Rightarrow \frac{\partial \nabla_{xy}}{\partial x} + \frac{\partial}{\partial y} \left(C_{yy} - V \right) = 0$$

$$\int_{NN} - V = \frac{\partial^2 f}{\partial y^2}, \quad \int_{NY} - V = \frac{\partial^2 f}{\partial n^2}, \quad \int_{NY} = -\frac{\partial^2 f}{\partial x \partial y}$$

$$O(1-i) \stackrel{?}{\sqrt{1-i}} + (1-i) \stackrel{?}{\sqrt{1-i}} \stackrel{?}{\sqrt{1-i}} = \stackrel{?}{\sqrt{1-i}}$$

$$\Rightarrow (1-i) \forall q = (1-2+2i) \forall v$$

$$\Rightarrow \forall q = -\frac{1-2i}{1-v} \forall v \rightarrow Plane Strain$$

$$\Rightarrow \forall q = -\frac{1-2i}{1-v} \forall v \rightarrow Plane Strain$$

$$\Rightarrow \forall q = -(1-i) \forall v \rightarrow Plane Strain$$

$$\Rightarrow \forall q = -(1-i) \forall v \rightarrow Plane Strain$$

$$\Rightarrow \forall q = 0 \rightarrow Torre \text{ for Plane Strain}$$

$$\Rightarrow \forall q = 0 \rightarrow Torre \text{ for Plane Strain}$$

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Polynomial solutions to the biharmonic equation

$$\nabla^4 \varphi = 0 \quad \Rightarrow \quad \frac{\partial^4 \varphi}{\partial x^4} + 2 \frac{\partial^4 \varphi}{\partial x^3} + \frac{\partial^4 \varphi}{\partial y^4} = 0$$

$$Q = \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} A_{mn} x^m y^n = A_{00} + A_{10} x + A_{01} y + A_{11} x^n y + A_{02} y^n + A_{$$

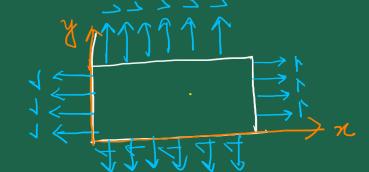
$$\int_{XX} = \frac{\partial^2 Q}{\partial y^2}, \quad \int_{YY} = \frac{\partial^2 Q}{\partial x^2}, \quad \int_{YY} = -\frac{\partial^2 Q}{\partial x^2}$$

Terms with m+n <1 > do not contribute strosses

Second-degree terms vill produce a cont. stress field

$$Q = A_{11} xy + A_{20} x^{2} + A_{02} y^{2}$$

$$\sigma_{xx} = 2A_{02}$$
, $\sigma_{yy} = 2A_{20}$, $\sigma_{xy} = -A_{11}$



Third degree terms will produce linear stress fild $\varphi = A_{30}x^3 + A_{21}x^3y + A_{12}xy^3 + A_{03}y^3$ J = 2A12 x + 6 A03 y $T_{y} = 6A_{30}x + 2A_{21}x$ $\frac{1}{2} = -2A_{21} - 2A_{12}$

Cowider the smple special case $A_{12} = A_{21} = A_{30} = 0$

Jxx = 6A03 }

Tyy = 0 Tny = 0 # Terms with min < 3 identically satisfy the biharmonic eyn Fox min; 3, special conditions involving the coefficients will have to be found.

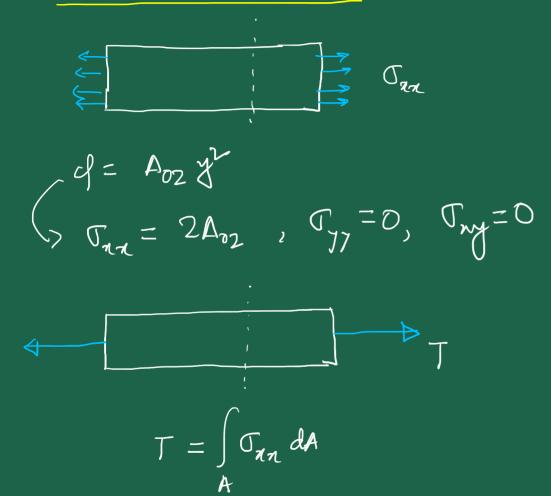
Principle of Superposition

Norks because the linear nature of the bhasmonic egn.

Hon-lin.

The Hon-lin.

St. Venant's Principle



For statically equivalent loadings the stress field is going to be the same as long as we stay from the endo.